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Morpho-structural criteria for the identification of spreading-induced deformation processes potentially comprising stratovolcano stability.

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2 **processes potentially comprising stratovolcano stability.**

3

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22 ABSTRACT

23 The characterization of stratovolcanoes' surface deformation is essential for a better understanding of the
24 processes that can compromise volcano structural stability and possible flank collapse. Morphological
25 similarities produce by volcano deformation due to the presence of an hydrothermal core and by the
26 intrusion of a viscous magma body, produce a pressing need for advancing in our understanding of
27 recognition criteria of stratovolcanoes flank spreading. We provide analogue models and real volcanoes
28 examples to characterize and recognize the surface deformation patterns produced by spreading due to the
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30 presence of an hydrothermal core and intrusion processes inside the volcano in: (1) a sharp transition
31 between areas of subsidence and uplift is typical of intrusion-related deformation; (2) the development of
32 faults with oblique strikes in the upper part occurs only at intrusion experiments; and (3) the development
33 of flank bulging close to the cone base only occurs during asymmetric flank spreading. However, although
34 laboratory results show different criteria representative of the spreading process, diagnostic ('forensic')
35 application to real volcanoes is difficult, as in most cases some diagnostic structures cannot be preserved.
36 The occurrence of "basal" bulging at an edifice arises as a potentially powerful diagnostic morphological
37 feature for the identification of an asymmetric volcano flank spreading potentially compromising
38 stratovolcanoes stability. Remote sensing techniques can allow the identification of such basal bulges,
39 providing an easy tool for a more complete hazard assessment and refined monitoring strategy at potentially
40 unstable volcanoes.

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49 INTRODUCTION

50 Catastrophic flank collapse can occur in any volcano type, independent of its composition, shape, size, or
51 geodynamic context (McGuire 1996; Acocella 2005; Carrasco-Nuñez et al. 2011). Interest has been given
52 to the instability and catastrophic flank collapse of stratovolcanoes, especially since Mt. St. Helens'
53 eruption in 1980 (e.g., Voight et al. 1983; Siebert 1992; Carrasco-Nuñez et al. 2011). Flank collapse at
54 stratovolcanoes must be considered a strongly hazardous process, both due to its ability to potentially
55 impact large areas (including those affected by secondary hazards, as tsunamis) and to its high temporal
56 frequency, having caused about 20,000 fatalities in historical times (Siebert et al. 1987). Since 1500 AD,
57 25 flank collapses involving a volume of material greater than 0.1 km³ have been recorded in
58 stratovolcanoes (Carrasco Nuñez et al. 2011): a frequency of 4-5 times per century.

59 From those 25 large historic volcanoes' catastrophic flank collapses, 16 were associated with a coetaneous
60 magmatic activity (64%), whereas 4 of them were related to phreatic explosions, and in 5 cases no explosive
61 component was identified (Carrasco-Nuñez et al. 2011). The close connection between magma intrusion
62 and catastrophic lateral collapse in volcanic edifices is confirmed in the geological record by numerous
63 examples where volcanic debris avalanche deposits contain juvenile magmatic clasts or directly overlie
64 nearly simultaneous explosive deposits (Belousov et al. 2007). However, even though most of the identified
65 volcanic flank collapses, including the historical cases, were induced by a magmatic intrusion (e.g., St.
66 Helens at 1980; Voight et al. 1983), the geological record also shows numerous examples of the occurrence
67 of volcanic debris-avalanche deposits with no magmatic component or eruptive deposit associated (e.g.,
68 the historic cases of Mombacho (Nicaragua) at AD 1540 or Unzen (Japan) at AD 1792; van Wyk de Vries
69 and Francis 1997; Siebert et al. 1987). The prime factors for stratovolcano instability in these cases of no-
70 magmatic collapses have been frequently related to other internal geological processes, such as: 1) the
71 action of faults underlying the volcanic edifice (e.g., Lagmay et al. 2000); 2) the asymmetric volcano
72 spreading over a weak basal layer (Borgia et al. 1992; Borgia and van Wyk de Vries 2003) or 3) the
73 development of a core of hydrothermally altered rocks inside the volcano (van Wyk de Vries et al. 2000).

74 Hydrothermal rock alteration probably plays a key role as a priming mechanism for stratovolcano instability
75 and lateral catastrophic collapses, as evidenced by: 1) the presence of hydrothermally altered material in
76 several volcanic debris avalanche deposits (e.g., Pevear 1982; Voight et al. 2002; Salaün et al. 2011), and
77 2) the association of hydrothermal explosions with several historical examples of catastrophic flank

78 collapse (Reid et al. 2001). For example, at the Bandai volcano (Japan) in AD 1888, successive phreatic
79 eruptions (up to 20 times a minute) occurred until the final one triggered the catastrophic collapse of the
80 volcano's northern flank (Sekiya and Kikuchi, 1980). The significant number of stratovolcanoes worldwide
81 showing surface evidence of a hydrothermal system inside (hot water and/or gases emissions,
82 hydrothermally altered zones) underlies the relevance of these processes in analysing potential collapse-
83 related hazards.

84 The role of hydrothermal alteration for making unstable a volcanic edifice is manifold. First, alteration of
85 the volcanic rocks can reduce the porosity and permeability of the rocks (Berger and Henley 2011; Horwell
86 et al. 2013) promoting the development of high pore fluid pressures within the volcanic edifice, which can
87 favour fracturing and therefore a loss of strength (Lopez and Williams 1993; Day 1996; Reid 2004; Heap
88 et al. 2021). Furthermore, hydrothermally altered rocks become mechanically weaker than fresh rocks due
89 to the development of secondary minerals (mainly clay minerals), which have low strengths and reduce
90 cohesion and friction values of the rock mass (Darmawan et al. 2020). In addition, altered rocks show a
91 tendency to deform mainly by ductile mechanisms, so the development of such a weak and ductile core of
92 hydrothermally altered rocks can promote the gradual spreading of the edifice (van Wyk de Vries et al.
93 2000; Cecchi et al. 2004). This ductile deformation can show very low-rates, challenging its detection by
94 geodetic monitoring techniques (InSar or GPS).

95 The understanding in stratovolcanoes subjected to hydrothermal activity of the factors that promote their
96 catastrophic flank collapse, as well as the identification of diagnostic deformation features, can save lives
97 and property. Some insights into the volcano instability process due to the development of a weak
98 hydrothermal core have been obtained from field observations (Rosas Carbajal et al. 2016), remote sensing
99 (Michon and Saint- Ange, 2008), rock mechanics (Zimbelman et al. 2003) and numerical modelling
100 (Kelfoun et al. 2021), but key contributions for the identification and understanding of this process have
101 come from analogue modelling (Cecchi et al. 2004; van Wyk de Vries et al. 2000; Andrade and van Wyk
102 de Vries 2010; Rincón et al. 2015; Rincón et al. 2018).

103 In this way, analogue modelling has shown that the development of a concave-convex shaped flank at
104 stratovolcanoes can be considered as one of the most characteristic diagnostic features of the occurrence of
105 a gradual asymmetric gravitational deformation of weak-cored edifices. For this reason, at several
106 volcanoes has been proposed as evidence of the flank spreading of the edifice (e.g., Semeru volcano,

107 Indonesia; Solikhin et al. 2012). However, analogue modelling, as well as observations of some historical
108 episodes (e.g., Bezymianny, Kamchatka, at 1959 or St. Helens, USA, in 1980), have shown that a
109 cryptodome intrusion can also produce the volcano flank bulging developing a concave-convex profile
110 (Donnadiu et al. 2003, Cecchi et al. 2004). Those deformation features, which can be potentially quite
111 similar to those proposed as diagnostic of an active flank spreading, can be preserved for some time in the
112 volcano surface (e.g., van Wyk de Vries et al. 2018); i.e., an old intrusion can potentially have shaped the
113 volcano a long time ago in a way that strongly resembles the morphology of an edifice suffering an active
114 flank spreading (Donnadiu et al. 2003).

115 For this reason, in order to improve our ability to identify if the deformation mechanism responsible for
116 flank bulging of a stratovolcano flank is an active slow spreading (i.e., undetected for monitoring systems)
117 or the past deformation due to an old intrusion, we propose that a set of diagnostic criteria is needed based
118 on the morphology and the deformation structures observable on the volcano surface. To constrain those
119 morphological diagnostic criteria, we have performed an experimental study using systematically
120 comparable analogue models of volcano deformation due to a weak core and a viscous magma intrusion.

121

122 3. EXPERIMENTAL METHODOLOGY

123 3.1. Experimental setup

124 We have made two different types of volcano deformation models: 1) Type S which recreates volcano
125 spreading process due to the existence of a hydrothermal weak core; and 2) Type I which recreates a
126 cryptodome (i.e., viscous magma) intrusion. A mixture of fine-grained sand (80%) and plaster (20%) has
127 been used to simulate the fresh rock of the volcanic edifice at both types of models. This granular material
128 is commonly used to modeling crustal volcanic rock and visualize brittle faulting (e.g., Merle and Borgia
129 1996; Delcamp et al. 2008; Rincón et al. 2015; Rincon et al. 2018). In both setups, the cones have been
130 constructed on a rigid base above a one-centimetre-thick layer of the same material as the cone, in order to
131 avoid the process of friction between the sand cone and the rigid surface (figure 1). In the first setup (type
132 S) the core formed by hydrothermally altered rock has been simulated with silicone FB GUM, following
133 the methodology of Cecchi et al. (2004). The second type of model (type I) reproduces magmatic intrusion
134 processes using syrup injected from the base of stratovolcanoes with the same methodology as Rincón et

135 al., 2018 (figure 1). We use a Microsoft® Kinect v2 sensor in all the experiments for monitoring the surface
136 deformation (Rincón et al. 2018, 2022) (figure 1).

137 In type S experiments, due to the diversity of possible shape, size, and locations of the hydrothermal cores
138 inside stratovolcanoes, we design of experiments set to systematically recreate spreading caused by the
139 presence of a hydrothermal core with different characteristics. We consider three different variables for the
140 weak core; (1) core shape: cube, prism and cone; (2) core size: large (10%) and small (5%); and (3) core
141 position: base - centre, medium - centre and base - side (Figure 2). The combination of these three variables
142 results in 17 possible different experimental settings that reproduce the different possible occurrences of a
143 weak core inside a volcano (Figure 2). In order to validate the reproducibility of these S experiments, the
144 experiment S6 has been repeated 9 times; the variability observed in the morphology and faults due to the
145 cone deformation is minimal and the main diagnostic features appear at all the test (Online Resource 1).
146 On the other hand, we have realized a set of 6 experiments of type I. The only variable in these experiments
147 was the distance between the intrusion tube and the central axis of the cone: we show here experiments
148 with distances less than 0.5 cm and distances between 1.5-3 cm. The results from the I-experiments
149 performed are alike to those obtained by Rincón et al. (2018).

150

151 3.2. Scaling and materials

152 In order to compare surface changes and faults patterns in the analogue models with field data in the natural
153 systems, scaling of the experiments needs to be geometrically, dynamically, and kinetically defined
154 (Hubbert 1937). For the scaling in this work, the method and the range of the parameters are the same used
155 by Rincón et al. (2018). The length scale $[L]^*$ is 10^{-4} (so 10 m in real volcanoes is 1 mm in the model). The
156 cone height (hM) is 11 cm, modelling an 1100 m edifice (hN). The cohesion of the model material (σ_M)
157 has been estimated by shear-ring test in HelTec Lab of GFZ Potsdam (Samaniego et al. 2015), obtaining
158 values of 50-100 Pa, which simulates a fresh rock mass with a cohesion (σ_N) of $9 \cdot 10^5 - 2 \cdot 10^6$ Pa ($\approx 1 - 2$
159 MPa) (Seisdedos et al. 2012).

160 To simulate the hydrothermally altered volcanic core we employ the Rhodorsil GUM FB® silicone because
161 of the tendency of the hydrothermally altered rocks to deform mainly by creep (van Wyk de Vries et al.
162 2000; Cecchi et al. 2004). The viscosity of Rhodorsil FB® silicone is $1 \cdot 10^4$ Pa·s (Calvin et al. 2013)
163 whereas the viscosity of a real hydrothermal core has been estimated around $1 \cdot 10^{18}$ Pa·s (van Wyk de Vries

164 and Matela 1998). In this way, one minute of a type S experiment corresponds to around 10,000 years at
165 nature. In our type-I experiments we used Lylle's Golden Syrup to simulate the intrusion of magmas with
166 viscosities around $1 \cdot 10^9$ Pa·s, like those proposed for the cryptodome of Mt. St. Helens in 1980 (Pinkerton
167 and Stevenson 1992). Therefore, and according to the defined scaling (Table 1), our model flows (Q_M) of
168 $\sim 2 \text{ cm}^3/\text{s}$ are properly modelling natural flows (Q_N) of $\sim 30 \text{ m}^3/\text{s}$, similar also to that of the Mt. St Helens
169 cryptodome intrusion at 1980 (Moore and Albee 1981).

170 3.3. Data analysis

171 Experiments are monitored using the RGB and distance images obtained by the sensor Kinect v2 of
172 Microsoft® (Rincón et al. 2020). We used the RGB images to map the deformation structures (faults). With
173 the distance images we can quantify the topographic changes of simulated stratovolcanoes throughout the
174 several temporal stages of the process. Spatial resolution are 1920×1080 pixels for RGB images and 512
175 $\times 420$ pixels for the distance images. Since we record data from a height of 75 cm, the pixel sizes are 0.6
176 mm and 1.6 mm respectively. Temporal resolution is 1 image per second recorded every 10 minutes during
177 type S experiments and 1 image per second until the syrup reached the surface at type I experiments.

178 To obtain quantitative values of the surface deformation (i.e. subsidence and/or bulge) of the cone during
179 the experiments, we calculate the difference between the values of the different acquired distance images
180 and that of the starting time of the experiment (t_0). For type S experiments we analyse the images of the
181 minutes 1 (t_1), 2 (t_2) y 3 (t_3), which correspond approximately to 10000, 20000, and 30000 years in nature,
182 according to scaling. The selected times for type I are 5 (t_5), 10 (t_{10}), and 20 (t_{20}) minutes in the
183 experiment, representing 6, 12, 19, and 25 days in nature approximately.

184

185 4. RESULTS FROM ANALOGUE MODELS

186 4.1. Deformation by spreading due to a hydrothermal weak core (S-type models).

187 Most of the S-type models show a visible deformation at the cone surfaces, both as topographic
188 displacements and faulting (Figure 3). The greater and closer to the surface is the weak core simulating the
189 hydrothermally altered rocks body, the larger and more intense is the surface deformation (Figure 3).
190 Surface morphology changes detected are mainly characterized by the subsidence of the summit area (up

191 to 15 mm), developing a characteristic summit flat (i.e., low-slope) area at the edifice (Figures 3 and 4). In
192 several experiments, this subsidence is accompanied by a partially surrounding zone of small positive
193 displacements which, even in those cases where the weak core is located centred in the cone, can show a
194 small asymmetry with larger developments in different flanks (see experiments S1, S2, S10, S11, S14 and
195 S17 at figure 3). Faulting pattern at most of those centred cases is symmetrical, with the development of
196 two main curved normal faults, bounding the subsidence zone, dipping to the centre of the cone forming a
197 summit graben structure (see experiments S1, S2, S10, S11, S14 and S17 at figure 3).

198 In most of the models where the weak core is located off-centre in the edifice, faulting pattern changes: an
199 early master curved normal fault, located at the flank opposite to the weak core, develops dipping inward
200 the edifice (Figure 3: all the off-centre experiments except S3). In the hanging wall of this master fault, one
201 or several minor antithetic normal faults develop generating a half-graben structure in a highly deformed
202 flank. In addition, a prominent (up to 25 mm of positive displacement) topographic bulge growth close to
203 the cone base downslope of the fault system, presumably related to the development of a blind gently
204 dipping inverse fault at its base. This bulged area extends for around 1/4 of the edifice diameter, as a
205 minimum, even for narrow weak-cores (e.g., experiment S12 at figure 3). Remarkably, the maximum
206 subsidence is again located at the cone summit area, although extending into the deformed flank. The
207 deformed flank develops a topographic profile with a characteristic concave-convex shape (see experiments
208 S3, S6, S9, S12, S15 and S18 at figure 4), which has been already suggested as indicative of volcano flank
209 spreading (van Wyk de Vries and Francis 1997; van Wyk de Vries and Matela 1998)

210 In summary, surface deformation in off-centre S-models shows a quite distinctive asymmetrical pattern:
211 intense faulting forming an asymmetrical half-graben affecting the upper-half part of the flank, which
212 downslope shows a prominent bulge near the cone base, resulting in a concave-convex shape of the cone
213 flank (see experiments S3, S6, S9, S12, S15 and S18 at figures 3 and 4). We suggest that the deduced
214 geometry of those faults inside the edifice results in a strong potential instability of that deformed flank,
215 which therefore becomes prone for its catastrophic lateral collapse.

216

217 4.2. Comparison with deformation due to the intrusion of a viscous magma body (I-type models).

218 Surface deformation patterns detected at cones affected by the intrusion of a simulated viscous magma body
219 shows several features apparently similar to those at S-models. In our I-type models deformation is also

220 different between cases where the tube intrusion is centred or off-centred respect to the cone summit, in
221 agreement with previous results from Rincon et al. (2018). When intrusion occurred right beneath the cone
222 summit, edifice faulting is mainly symmetrical with two main inward-dipping normal faults forming a
223 summit graben, characterized by subsidence surface displacements. In some cases, the footwall zone of one
224 of the faults delimiting the graben also shows a small positive displacement (i.e., bulging. See experiment
225 I33, I35 e I44 at figure 5). That deformation pattern is quite similar to that from the S-models with the weak
226 core centred inside the cone (see experiments S1, S2 at figure 3)

227 However, in the cases when the intrusion occurs below one flank (i.e., off-centre), cone deformation shows
228 a completely different pattern, with the early development of a curved normal fault perpendicular to the
229 intruded flank dipping inward the volcano, producing a summit asymmetric half-graben with large and
230 strong (up to 25 mm) subsidence at the master fault hanging wall. The maximum subsidence zone can
231 therefore occur not at the cone summit zone, but slightly displaced (i.e., above of the intrusion point) (see
232 experiments I4, I18 and I40 at figure 5). Remarkably, a topographic bulge appears at the intruded flank, in
233 sharp transition with the subsidence zone (in some cases clearly bounded by one the graben faults), and
234 therefore always at the upper-middle zone of the flank, but not at the cone base (see topographic profile of
235 experiment I4 at figure 6). This deformation pattern can be therefore very similar to that from some of the
236 off-centre S-models, except in the location of the bulge (upper-middle flank vs. cone base) (e.g., experiment
237 S12 at figure 4 vs experiment I4 at figure 6).

238 Another remarkable deformation characteristic observed in these off-centred I-models is the development
239 at the hanging-wall block of normal faults trending $\approx 30^\circ$ respect to the first master fault (see experiments
240 I4 and I18 at Figure 5). This faulting pattern appears at advanced times of the experiment. Occasionally,
241 also a late “slump-like” structure develops, defined by a U-shaped normal fault and a prominent bulge,
242 trending highly oblique to the first larger master fault (see experiments I4 and I40 at Figure 5).

243 5. DISCUSSION

244 5.1. Morpho-structural features indicative of potential volcano instability due to flank spreading.

245 Our S-type experiments, simulating the gravitational deformation of a stratovolcano with a weak core of
246 hydrothermally altered rocks, show how a volcanic edifice can spread developing faulting patterns which
247 potentially can compromise its stability: a normal master fault involving a large portion of the edifice,
248 including a strongly deformed flank. This asymmetrical unstable deformation of the volcano by preferential

249 flank spreading is only observed in some of the models where the weak core is located off-centred, in
250 agreement with results from previous models of Cecchi et al. (2004). Additionally, our models show that
251 this volcano deformation can occur even when the weak hydrothermally-altered core is only 5% in volume
252 in the edifice (10% for Cecchi et al. 2004), showing that even quite small hydrothermal systems can
253 potentially generate instability in stratovolcanoes.

254 One of the most characteristic topographic features observed in our models due to the cone spreading over
255 its weak core is the development of a flat (low-slope) summit area due to edifice subsidence. That flat
256 summit area could therefore potentially become a good evidence for identifying the spreading of a
257 stratovolcano. However, that graben-like flat area can be difficult to identify since lava flows from central
258 vent can infill it and even cover and mask the topographic scarps produced by faulting. In any case, since
259 both the symmetrical and asymmetrical (i.e., restricted to a flank) spreading of the edifice produce
260 subsidence at the summit area, this criterion is not useful for the identification of a potential instability of a
261 stratovolcano. Similarly, if the deformation of the volcano was due to an old intrusion of a viscous magma
262 body, our I-models show that a graben-like flat area due to topographic subsidence develops also at the
263 cone summit zone. The occurrence of a flat summit area in a stratovolcano is therefore a useless criterion
264 for characterizing volcano deformation process.

265 Otherwise, other topographic characteristic diagnostic of volcano deformation detected in our experiments,
266 the flank bulging signature, can be detected even if later lava flows cover the area, due both to the change
267 in slope and also by the potential change in morphology of the later flows reaching the slope-change area.
268 Both flank spreading and intrusion processes can produce a bulge at the edifice (see Figures 3, 4, 5 and 6).
269 Our results show that a fault-related sharp transition between subsidence and uplift at deformed volcano
270 flanks is typical of intrusion-related deformation. This distinctive feature occurs in all our experiments,
271 strengthening the proposal made by Donnadieu et al (2003) using only one experiment as well as previous
272 field observations (e.g., van Wyk de Vries et al. 2014).

273 In addition, our I-type experiments show that the deformation due to a viscous magma intrusion high in the
274 edifice can derive in a characteristic and diagnostic faulting pattern, with the development of faults with
275 different strikes crosscutting in the upper part of the deformed flank (Figure 5). This faulting pattern appears
276 therefore as a potentially very powerful criterion for the recognition of past edifice deformation by an old
277 intrusion, and therefore for discarding an active volcano flank spreading in an edifice which shows

278 morphological features such as a flat summit area and a concave-convex flank. However, we have no found
279 evidence of that faulting pattern at any volcano worldwide, neither at our analysis of satellite images (see
280 Section 5.2.) nor at the scientific literature. This faulting pattern occurs in our experiments at a late stage,
281 when the intrusion is probably located high in the edifice above the main fault plane, and therefore the
282 volcano is in a highly unstable stage (Rincón et al., 2018). Therefore, we propose that this faulting pattern
283 is highly improbable to be preserved at stratovolcanoes at nature due to the probable catastrophic lateral
284 collapse of the edifices at those situations.

285 Finally, the comparative analysis of our S- and I-type models shows that the volcano flank bulging close to
286 the cone base only occurs in those cases where the edifice is suffering an asymmetric spreading (see
287 experiments S6, S9, S12, S15 and S18 at Figures 3 and 4). The development of “basal” bulging of the
288 edifice arises therefore as a diagnostic morphological feature for the identification of an asymmetric
289 volcano flank spreading which potentially can be compromising the edifice stability in that sector

290

291 5.2. Application to natural cases

292 Volcano flank bulging, with the development of a characteristic concave-convex-concave profile at the
293 edifice deformed flank, has been previously proposed as a morphological criteria for identifying the
294 development of flank spreading at several volcanoes; e.g.: Casita (van Wyk de Vries et al., 2000),
295 Mombacho (Cecchi et al., 2004), Piton de la Fournaise (Carter et al., 2007), Teide (Márquez et al., 2008),
296 Semeru (Solikhin et al., 2012) or Damavand (Eskandari et al., 2015). The surface occurrence of
297 hydrothermally altered rocks at several of those volcanoes (Casita, Teide, Damavand) strongly supports
298 that the volcano flank spreading can be produced by the existence of a core of weak rocks in the edifice.
299 Applying our described morphological criteria to proposed examples of volcano flank spreading some
300 noticeable features appear, in some cases providing new arguments for the existing controversies about the
301 role of flank spreading.

302 At Casita volcano (Nicaragua) the topographic profile across the proposed deformed east flank (van Wyk
303 de Vries et al., 2000) shows strong similarities to some of our cases of spreading due to a weak core located
304 centred in the cone, with a convex part located at the middle flank (Figure 8). That structural setting is not
305 potentially such unstable as the case where the weak core is located off-centre in the volcano. Even through,
306 the induced flank steeping and head scar faulting can produce small landslides which can transform into

307 small debris avalanches or lahars, as occurred at the edifice SE flank at 1998 (Kerle & van Wyk de Vries,
308 2001). That landslide left a small horse-shoe scarp in the volcano flank (Figure 8

309

310 Damavand volcano (Iran) shows some similar features, with a a characteristic concave-convex-concave
311 shaped SE flank (Figure 8) bounded at the north by a shallow horse-shoe scarp. That E-SE flank of the
312 edifice is actively deforming several millimetres per year to the west-down at the upper concave flank
313 sector, and west-down at the convex zone, according to InSAR data (Shirzaei et al., 2011; see their Figure
314 3). That deformation pattern is similar to that occurring in our models with a small off-centred weak core
315 (see e.g., S6 or 18 at Figure 3). These observations suggest that Damavand south-eastern flank can be
316 potentially unstable due to an asymmetric flank spreading process, constituting a threat of possible collapse
317 for the village of Ask and other localities at the Haraz River valley at the south-east foot of the volcano.
318 The morphology of the edifice flank also supports the proposal of Cecchi et al. (2004) that some of the
319 shallow horse-shoe structures occurring at volcano flanks can have been induced by flank spreading and
320 thus become a diagnostic feature of edifice deformation and instability.

321 According to our models, Semeru volcano (Indonesia) stability can be compromised due to south-directed
322 flank spreading, since the alleged bulge is located close to the base of the edifice flank (figure 8; see also
323 Figure 9 of Solikhin et al., 2012). However, after our inspection of volcano slope map, we have further
324 doubts about the existence of a deformation-related bulge at the edifice base, since the change-in-slope
325 defining the alleged southern bulge is quite small, discontinuous and lobate; i.e., it is not extended across a
326 significant part of the edifice base.

327 Additionally, we have made a preliminary survey using bibliography and the worldwide available SRTM
328 and Aster-DEM digital elevation models, looking for other possible examples of stratovolcanoes showing
329 morphological features potentially indicative of flank spreading (i.e., concave-convex-concave flanks,
330 possibly related to shallow horse-shoe structures). The most notable example found is Ubinas volcano
331 (Ecuador), where also a concave-convex-concave shaped flank (with an area $\sim 2 \times 1$ km) bounded by a
332 horse-shoe scarp occur at volcano southeast side (Figure 8). The horse-shoe scarp is attributed to the
333 occurrence of a large sector collapse occurred at the volcano around 3,670 yr. B.P. involving
334 hydrothermally altered blocks (Thouret et al., 2005). Ubinas edifice has a well-developed hydrothermal
335 system with a south-eastern trend asymmetric distribution (Gonzales et al., 2014). In fact, Ubinas is

336 considered a highly unstable volcano at its south flank, and the possibility of a flank failure of that
337 hydrothermally-altered zone affecting the area of the previous collapse is yet considered in the possible
338 eruptive scenarios in the hazards assessment (Thouret et al. 2005). However, it must be noted that the
339 morphology and structure of the flank adjacent at the NE to the horse-shoe scarp fit with our models where
340 a large off-centre weak-core is located inside the cone (see e.g. models S9 or S15 at Figure 3, compared to
341 profile at Figure 8). This suggests that the area where volcano stability can be compromised is larger than
342 the considered at the current volcano hazards map (Thouret et al. 2005, Rivera et al. 2010), and that a flank
343 collapse of a larger sector of the SE flank, including the area upslope of the Ubinas town, constitutes a
344 hazard that must be considered. Therefore, even although the previous monitoring of possible volcano flank
345 deformation at Ubinas using InSar techniques have not shown any signal (e.g., Rivera et al., 2010) we
346 suggest that the detailed monitoring of a potential slow long-term gravitational deformation at this SE
347 volcano flank is required due to the high potential hazard of a large catastrophic lateral collapse suggested
348 by the volcano morpho-structural criteria.

349

350 6. CONCLUSIONS

351 - Our experiments show that both the existence of a hydrothermal altered weak core or the intrusion
352 of a viscous magma body can produce two different deformation patterns at stratovolcanoes,
353 symmetric and asymmetric. Asymmetric deformation patterns can induce the instability of the
354 deformed volcano flank volcano producing structures that potentially can trigger its catastrophic
355 collapse.

356

357 - We identify three morpho-structural criteria which can potentially discriminate between
358 asymmetric volcano deformation due to spreading by a weak hydrothermal core or by intrusion of
359 a viscous magma body: (1) a sharp transition between areas of subsidence and uplift is typical of
360 intrusion-related deformation; (2) the development of faults with oblique strikes crosscutting in
361 the upper part of the deformed flank occurs only at intrusion experiments; and (3) the development
362 of flank bulging close to the cone base only occurs during asymmetric flank spreading.

363

364 - Diagnostic application of these criteria to natural cases seems to be hampered due to the usual
365 catastrophic lateral collapse of the stratovolcanoes deformed by off-centred viscous intrusions,
366 which erased the late-stage characteristic faulting patterns observed in our experiments.

- 367
368 - The development of “basal” bulging of the edifice arises therefore as the main diagnostic
369 morphological feature for the identification of an asymmetric volcano flank spreading potentially
370 compromising stratovolcanoes stability.
- 371
372 - The search and characterization of such basal bulges at stratovolcano flanks by remote sensing
373 techniques can provide an easy tool for a more complete hazard assessment and refined monitoring
374 strategy at potentially unstable volcanoes.

375

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379

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553

554

555 **FIGURES**

556 **Fig 1** Experimental setup. (A) type S volcano spreading by hydrothermal core and (B) Type I cryptodome
557 intrusion. A tripod with the Kinect sensor attached is located at a height of 0.75 meters above the table with
558 the experiment. The data obtained by the Kinect sensor is sent in real time to a data computing system

559 **Fig 2** Sketches of the different experiments produced by the combination of simulated hydrothermal system
560 parameters (shape, size, and location). The combination resulting for a hypothetical experiment S8 (in red)
561 is logistic impossible

562 **Fig 3** Results from spreading by hydrothermal core experiments (type S). Variation of the distance images
563 at time t3 (3 minutes in the experiment ~ 30,000 years in nature), with the deformation structures overlaid.
564 Lines a-b show the location of the profiles of figure 4

565 **Fig 4** Red line: topographic profiles of the S-type experiments at time t3 (3 minutes in the experiment ~
566 30,000 years in nature), compared with initial experiment profiles (black line). Grey figures: weak-core
567 geometry at the starting of the experiment

568 **Fig 5** Results from cryptodome intrusion experiments (type I). Variation of the distance image from time
569 t20 (20 minutes in the experiment ~ 25 days in nature), with the deformation structures overlaid. Lines a-
570 b show the location of the profiles of figure 6

571 **Fig 6** Two representative examples of type I experiments. Red line: topographic profiles at time t20 profile
572 (20 minutes in the experiment ~ 25 days in nature) compared with initial experiment profiles (black line)

573 **Fig 7** Sketches of the characteristics fault patterns and topographic changes (subsidence in blue, uplift in
574 red) detected at (A) Spreading experiment when the hydrothermal core is centred (B) Cryptodome intrusion
575 when the tube intrusion is centred (deformation pattern 1 of Rincón et al. 2018) (C) Spreading experiment
576 when the hydrothermal core is off – centred and (D) Cryptodome intrusion when the tube intrusion is off-
577 centred (deformation pattern 3 of Rincón et al. 2018)

578 **Fig 8** Topographic profiles (from SRTM and Aster-DEM data) of studied natural cases of stratovolcanoes
579 showing potential flank deformation due to edifice asymmetric spreading over a weak hydrothermally-
580 altered core. Red line marks the location of the proposed flank bulge analysed at each case

581

582 **TABLES**

583 **Table 1** Scaling: Geometrical and mechanical parameters of scaling and their values in nature and model

584

585

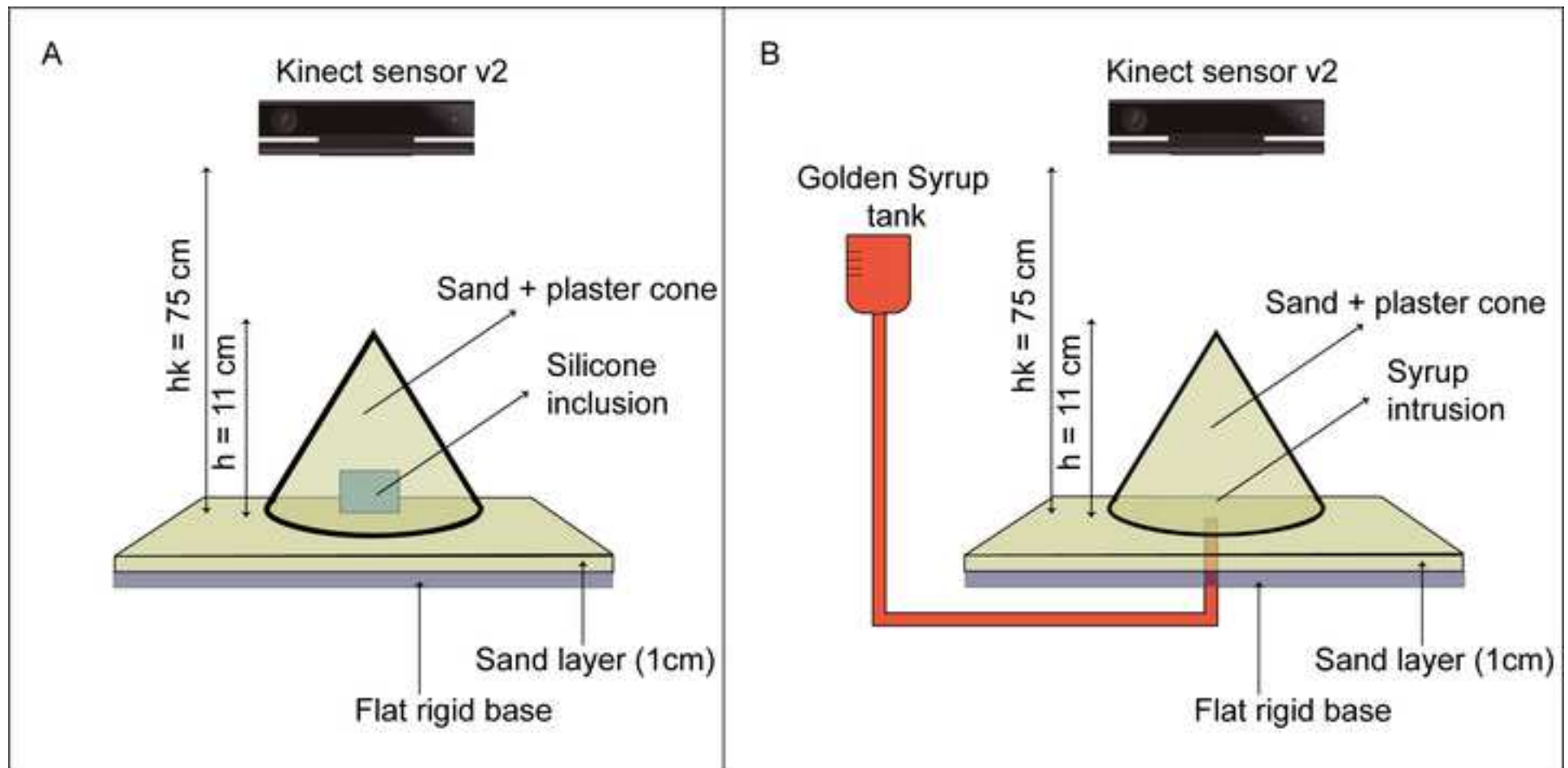
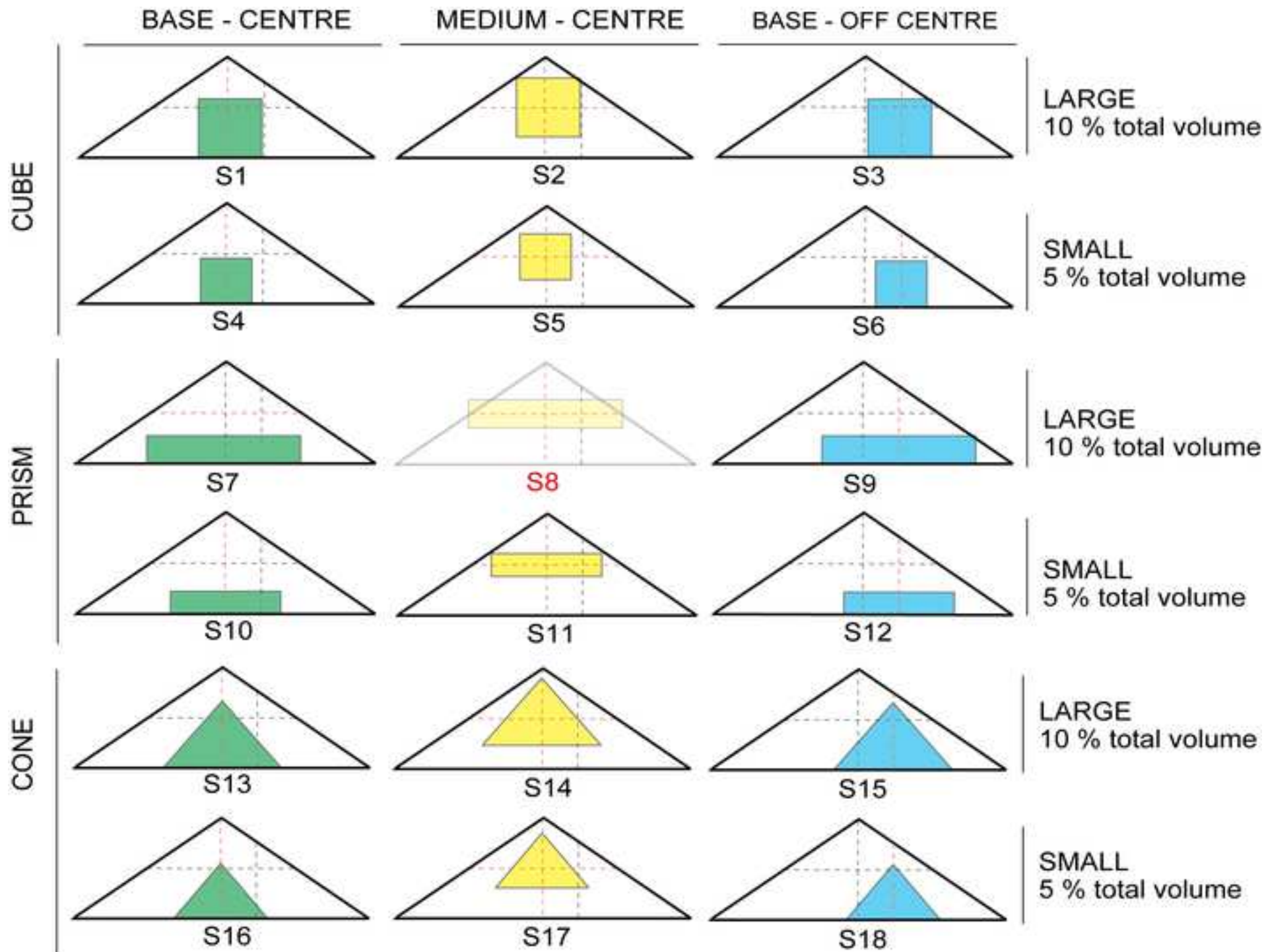


Figure 2



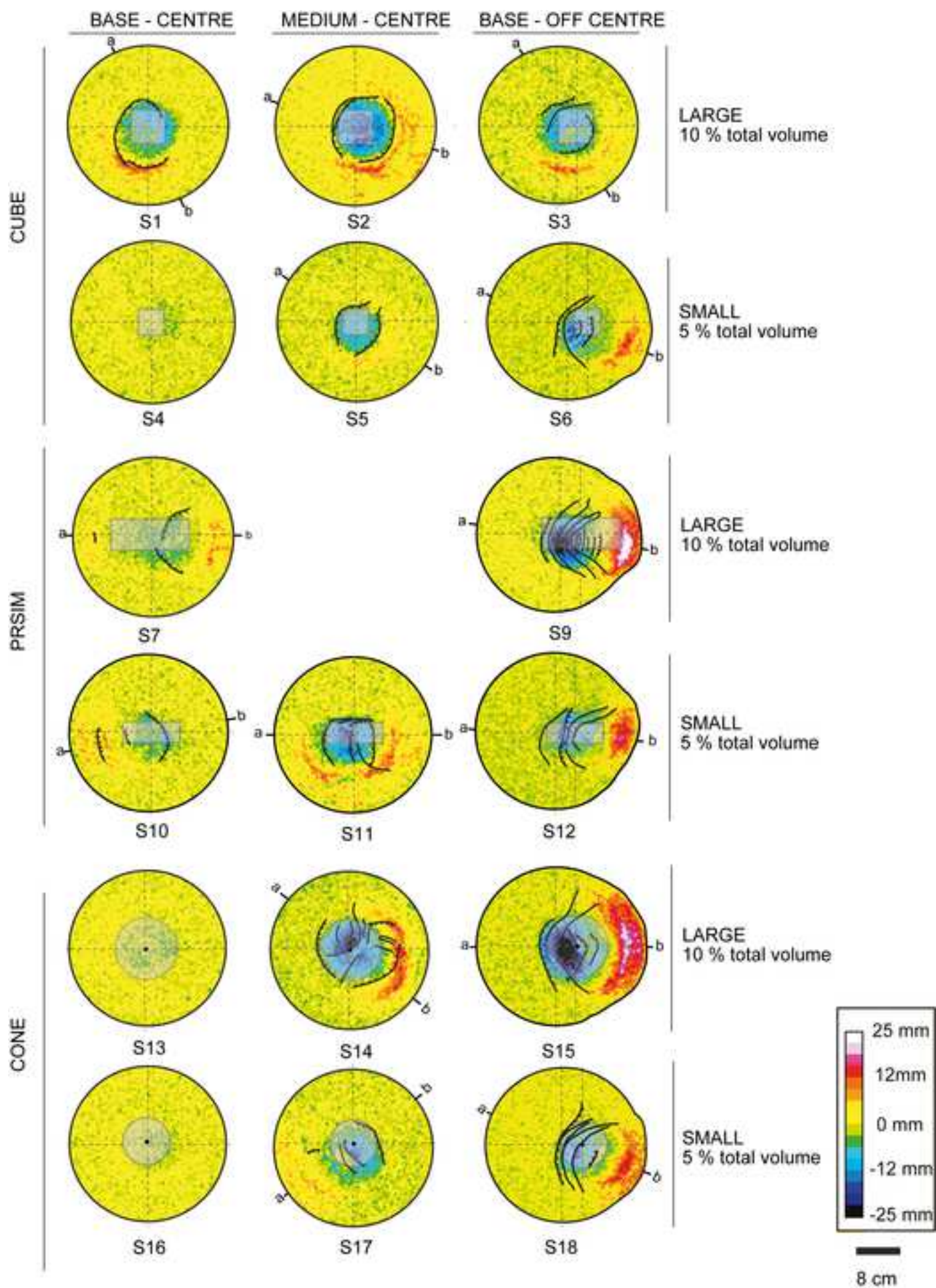
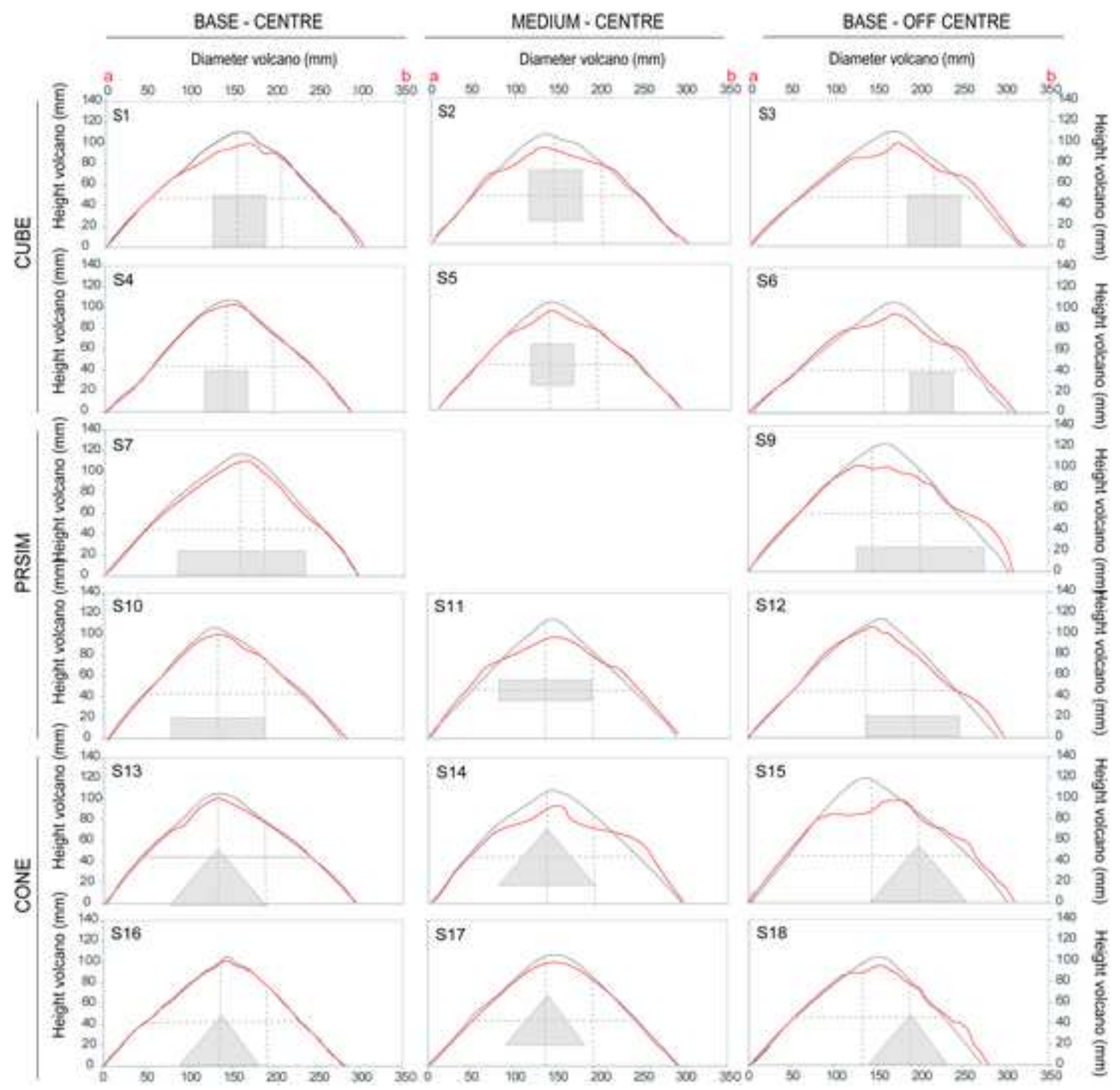


Figure 4



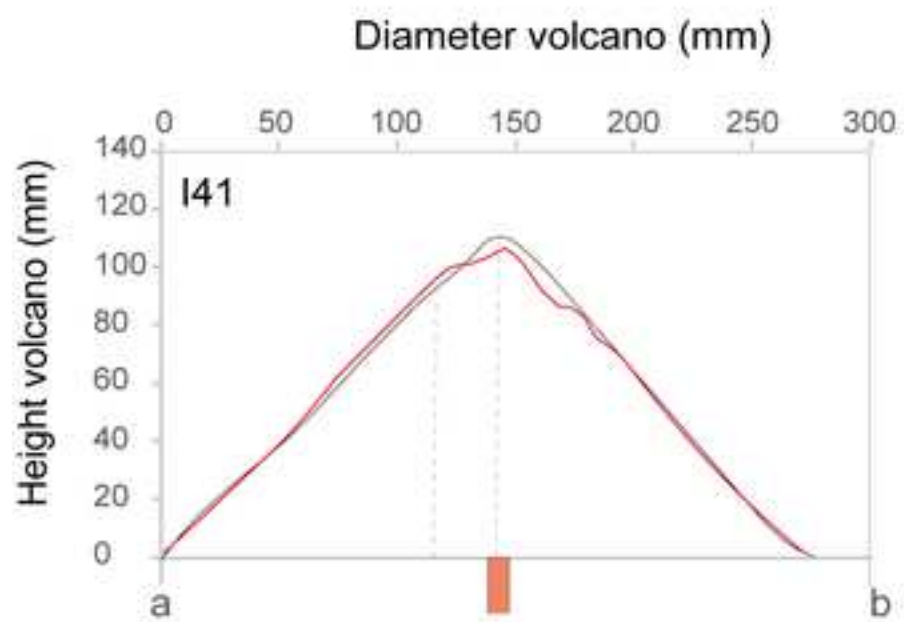
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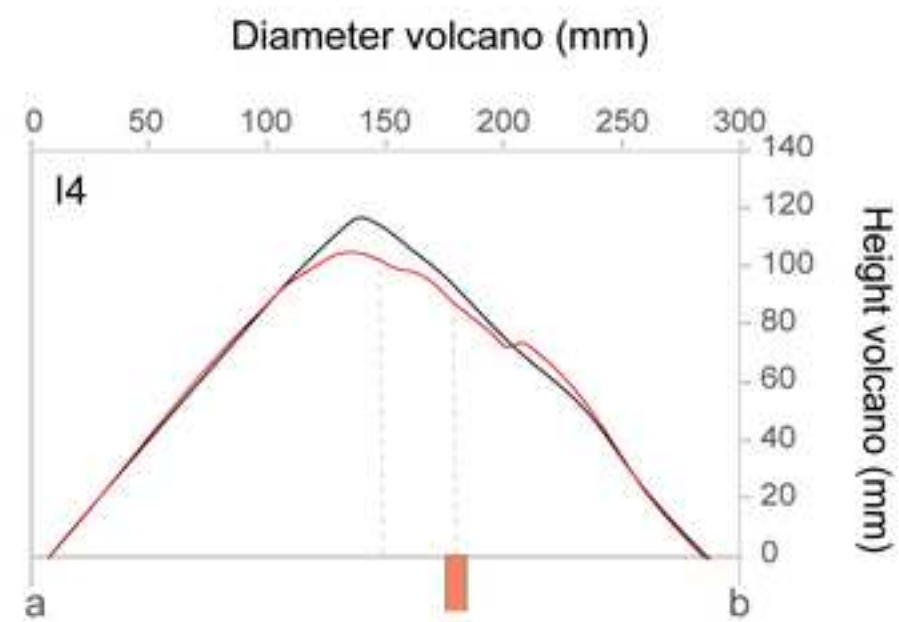
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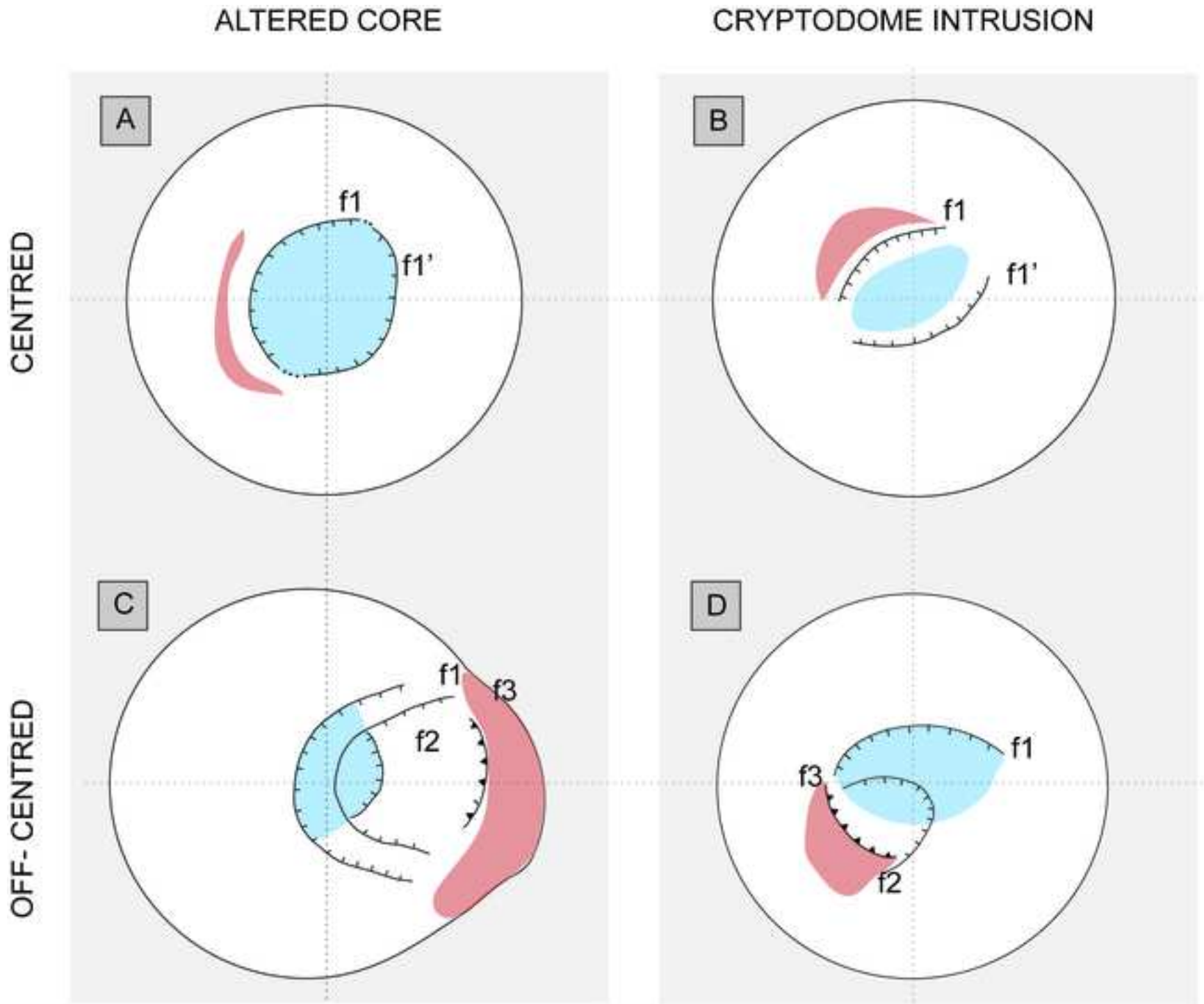
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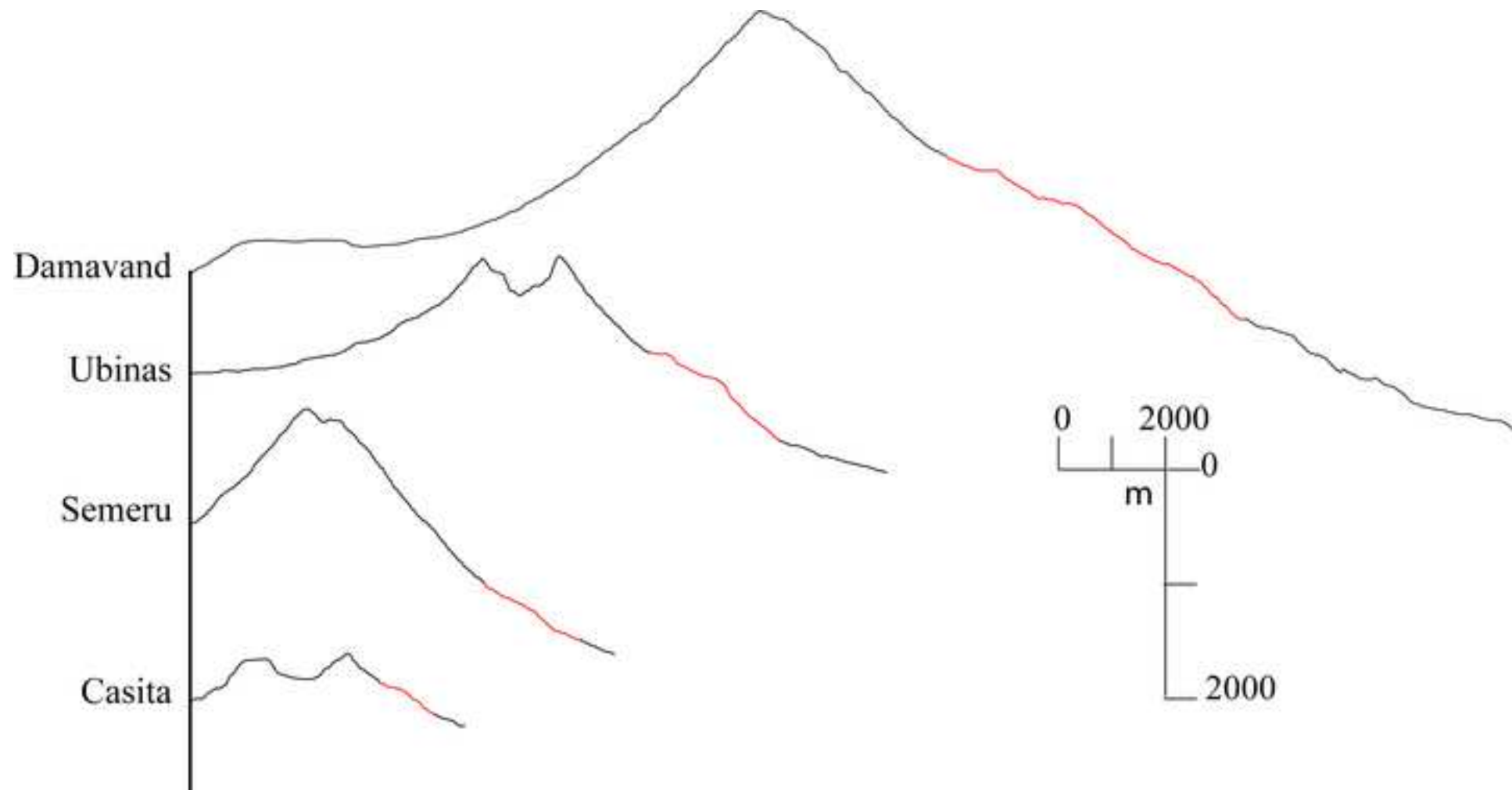


Table 1

Parameters	Definition	Model (M)	Nature (N)	Ratio (M/N)	Units (IS)	Dimensions
h	Stratovolcano Height	0.11	1100	1×10^{-4}	M	[L]
R	Stratovolcano radius	0.15	15000	1×10^{-5}	M	[L]
g	Gravity	1	1	1	$\text{m} \times \text{s}^{-2}$	$[\text{L} \times \text{T}^{-2}]$
ρ_v	Stratovolcano density	1320	2500	5.5×10^{-1}	$\text{kg} \text{ m}^{-3}$	$[\text{M} \times \text{L}^{-3}]$
σ_v	Stratovolcano cohesion	50 - 100	9×10^5	2.5×10^{-6}	$\text{kg} \times \text{m}^{-1}$	$[\text{M} \times \text{L}^{-1}]$
Φ	Friction angle	36-37	36-37	1	°	-
ts	Deformation time spreading	0-600	$0 - 3.2 \times 10^{12}$	$0 - 1.9 \times 10^{-10}$	S	[T]
ti	Deformation time intrusion	0-1.200	$0 - 2.2 \times 10^6$	$0 - 5.5 \times 10^{-4}$	S	[T]
μ_{sh}	Hydrothermal core viscosity	1×10^4	1×10^{18}	1×10^{-15}	$\text{kg} \times \text{m}^{-1} \times \text{s}^{-2}$	$[\text{M} \times \text{L}^{-1} \times \text{T}^{-2}]$
μ_m	Magma viscosity	30	1.5×10^9	3.3×10^{-9}	$\text{kg} \times \text{m}^{-1} \times \text{s}^{-2}$	$[\text{M} \times \text{L}^{-1} \times \text{T}^{-2}]$
Qm	Magma flow	1.7×10^9	1-100	1.5×10^9	$\text{m}^{-3} \times \text{s}$	$[\text{L}^{-3} \times \text{T}^{-1}]$



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